



# Article Application of the Gaussian Model for Monitoring Scenarios and Estimation of SO<sub>2</sub> Atmospheric Emissions in the Salamanca Area, Bajío, Mexico

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Abstract: Population and industrial growth in Mexico's Bajío region demand greater electricity consumption. The production of electricity from fuel oil has severe implications on climate change and people's health due to SO<sub>2</sub> emissions. This study describes the simulation of eight different scenarios for SO<sub>2</sub> pollutant dispersion. It takes into account distance, geoenvironmental parameters, wind, terrain roughness, and Pasquill-Gifford-Turner atmospheric stability and categories of dispersion based on technical information about SO<sub>2</sub> concentration from stacks and from one of the atmospheric monitoring stations in Salamanca city. Its transverse character, its usefulness for modeling, and epidemiological, meteorological, and fluid dynamics studies, as suggested by the models approved by the Environmental Protection Agency (EPA), show a maximum average concentration of 399  $\mu$ g/m<sup>3</sup>, at an average distance of 1800 m. The best result comparison in the scenarios was scenery 8. Maximum nocturnal dispersion was shown at a wind speed of 8.4 m/s, and an SO<sub>2</sub> concentration of 280  $\mu$ g/m<sup>3</sup> for stack 4, an atypical situation due to the geography of the city. From the validation process, a relative error of 14.7 % was obtained, which indicates the reliability of the applied Gaussian model. Regarding the mathematical solution of the model, this represents a reliable and low-cost tool that can help improve air quality management, the location or relocation of atmospheric monitoring stations, and migration from the use of fossil fuels to environmentally friendly fuels.

Keywords: simulation; Gaussian model; dispersion; emissions; meteorological variables; coefficients

## 1. Introduction

The field of environmental management and healthcare has focused attention on air quality, this focus revolves around the common problem experienced by a significant number of cities around the world due to the effects of atmospheric pollutants [1]. Studies in these fields have essentially focused on industrial cities whose dynamics imply an increase in pollution that is main produced by industry and motor vehicles [2]. Air pollution is considered a serious phenomenon due to its global character and a public health problem [3]. Therefore, these studies have permanently highlighted technical and epidemiological factors.



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**Copyright:** © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). It is important to increase the knowledge related to atmospheric emissions, their causes, dispersion mechanisms, and effects on the environment and health [1,4,5]. Yearly air quality reports by the World Health Organization (WHO) indicate that permissible limits of regulations are being exceeded, especially in Southeast Asia, Latin America, and the Caribbean [6]. To a greater extent, this is due to a lack of economic resources and effective strategies to repeatedly deal with atmospheric pollutants, which is alarming. In 2016, Mexico ranked second in deaths due to air pollution in Latin America, with around 9300 deaths. Brazil ranked second, with 23,000 deaths in the same period [7]. Table 1 shows the normative values stated in the WHO's Mexico Guidelines and their regulatory SO<sub>2</sub> standard.

Pollutant	WHO Guideline Value μg/m <sup>3</sup>	Period Used for the Assessment (h)	Indicator NOMs (Mexico) µg/m <sup>3</sup>	NOM (Official Mexican Standard, Official Journal of the Federation, DOF 2010)
SO <sub>2</sub>	20 on 24 h 500 on 0.166 h	24 8	288 on 24 h 66 annual average 524 on a daily average (must not be exceeded twice a year)	NOM-022-SSA1-2010

Table 1. Normative values for SO<sub>2</sub> standard WHO's Mexico guidelines.

The values of the Mexican standard for activation of environmental contingencies use the 24 h average. Source: Adapted from Greenpeace, 2018, p.12 [8].

Population and industrial growth in Salamanca city and some surrounding cities, which are part of the industrial corridor, the Bajío area, have caused an increase in electricity demand. However, the polluting gases emitted impact the environment and health [9]. According to Pacsi [10], more than half of the population are exposed to high pollution levels up to 2.5 times those recommended by WHO. The ProAir program (Swegon, las Rozas Madrid, Spain), at different times, has managed to implement strategies to decrease such industrial emissions. However, such strategy is challenged by the frequent environmental pre-contingencies that occur periodically. Among the criteria, the most common pollutants present in the air from the power generation industry are  $SO_2$ ,  $NO_2$ , CO, and  $PM_{10}$  [11]. The last update on Guanajuato State Pollutants Criteria and Precursors Inventory revealed the importance of monitoring the electricity generation industrial sector to assess its impacts and possible steps to be take in the short- to medium-term to protect the population's health against harmful pollutants. At the state level, in 2017, Salamanca city registered 87.8% of SO<sub>2</sub> emissions, which is equivalent to 16,661 ton/year, of which 15,778 and 781 ton/year corresponded to the petrochemical industry and the electricity generation sector, respectively [12].

According to Guanajuato's Ecology State Institute [13], non-compliance with  $SO_2$  and  $PM_{10}$  regulatory standards is the principal factor that causes environmental pollution precontingencies in industrialized municipalities with considerable mobility, such as the region studied. The national air quality report [14] indicated that, in Salamanca, the minimum number of days that exceeded some norm between 2000 and 2017 was 48, and the maximum was 175. In the same way, this indicates that in 2017, the number of pollutants that exceeded the maximum on 1, 2, and 3 days simultaneously was 77, 13, and 3, respectively. Sulfur dioxide (SO<sub>2</sub>) is a colorless gas with an irritating odor. Practically, 50% is deposited on the surface, presenting a short half-life in the atmosphere. Its reducing power converts it into SO<sub>3</sub>, which, due to its high solubility with air humidity, transforms into sulfuric acid (H<sub>2</sub>SO<sub>4</sub>), an acid rain component [15]. Because of its potential hazard, it belongs to the pollutant category criteria [16]. According to Economic Commission for Latin America and the Caribbean (ECLAC 2004), the fuel for thermal power plants

(TPPs) required for electricity production processes contains between 3.5% and 4% sulfur. According to data from the most recent update of Guanajuato's pollutant inventories, the principal source of SO<sub>2</sub> emissions was the oil and petrochemical sector, with 90.9% of the total emissions, followed by the electricity generation industry, with 4.5% of the total emissions [17]. Figure 1 shows the historical SO<sub>2</sub> emissions in Salamanca city from 2000 to 2017 monitored by Red Cross Station. The trend of the daily data is presented through the 10th and 90th percentiles, average and the maximum during the analysis period mentioned [18].



**Figure 1.** Emissions of  $SO_2$  in Salamanca 2000–2017. Source: Adapted from INECC [18]. Note: Upper light gray indicates the maximum level of  $SO_2$  emission, dark gray shows the percentile 90th; the band gray below shows the average and finally the dark band indicates the 10th percentile of emissions registered by the red cross station during the signal period.

In this context, this study aimed to simulate SO<sub>2</sub> dispersion from TPP chimneys to analyze the concentration profile from the emission point to the urban area, thus providing an approximation of the risk factors relating to health and the environment. The industrial chimneys of the Salamanca TPP are slender structures constructed with different materials, geometries, and dimensions for the evacuation of gases and fumes during the chemical process. This ensures the dispersion of SO<sub>2</sub> effluents into the atmosphere to comply with the environmental regulations of the area where the source is located. NMX-AA-107-1988 established a minimum height for chimneys, which must not exceed the elevation of the formed turbulence zone of the surroundings due to the effects of wind on buildings or mountains and trees near the installation [18,19]. The same standard recommends that the inner diameter regulates the exit speed of gases to be between 15 and 25 m/s [20].

In the area of effluent pollutant dispersion, it is common to use the term plume or plumes to designate the column or cloud of effluent that exits a stack and is incorporated into the atmosphere [21]. Dispersion is the diffusion of atmospheric pollutants emitted by industrial processes. Its intensity is associated with various technical factors, such as the diameter and height of chimneys; speed and temperature of the gas effluent; meteorological factors, such as pressure, atmospheric temperature, wind speed, and direction [22]; and, finally, it is also a function of the topographic conditions (space) of the emission source and time [23], as shown in Table 2.

Variable	Choices			
	Direction			
Wind	Persistence			
	Turbulence			
	Ground roughness			
	Urban areas			
Topography	Coast areas			
	Rugged terrain			
	Presence of buildings and obstacles			
	A = Extremely Unstable			
	B = Unstable			
Atmospheric Stability	C = Slightly Unstable			
Coefficient (ASC)	D = Neutral			
	E = Slightly stable			
	F = Stable			

Table 2. Geoenvironmental parameters.

The forms of pollution control suggested by the Environmental Protection Agency (EPA) include monitoring, which is diverse in terms of fixed or mobile technology [24], inventories, and modeling. Atmospheric dispersion models are an important tool for air quality management [25]. Simulation includes the latest knowledge on atmospheric dynamics to estimate the dissipation patterns, chemical reactions, and removal of such pollutants [26,27]. The numerical simulation of such phenomena models the dispersion and transport processes starting from data from the emitting sources. Other approaches employ advanced techniques, such as machine learning methodologies from different urban areas [28]. The mathematical description of pollutant transport in the atmosphere can be achieved using a parabolic-type second-order partial differential equation. In probability and statistics, the Gaussian distribution is used to analyze real events. In this particular case, the pollutant plume concentration depends on two longitudinal dimensions: the wind direction and the height of the plume. The mathematical model's solution is a function of the technical parameters of the stack and atmospheric emissions, meteorological factors (wind speed, atmospheric temperature, and pressure), and ground roughness [29].

## 2. Gaussian Model Application (Simulation Method)

Simulation of 8 different  $SO_2$  dispersion sceneries of 4 chimneys was performed in the Salamanca TC. It was performed by applying a Gaussian model, by means of the function of the x-distance, measured from the stack base in the motion direction of the pollutant plume.

#### 3. Study Area

Salamanca's municipality and city are part of Guanajuato State's most important industrial region, in the El Bajío industrial corridor. Economic relevance lies in the petrochemical industry, including a refining, chemical, automotive, and thermoelectric power plant. It has an area of 756.54 km<sup>2</sup> and is located at 20° 34 13″ N latitude and 101° 11 50″ W longitude at an altitude of 1721 m above sea level. According to the Instituto Nacional de Estadística, Geografía e Informática, INEGI, it has 273,271 inhabitants [30]. The ONU HABITAT indicated that Salamanca's municipality is in the basic index of prosperous cities but faces serious problems of atmospheric pollution due to emissions from the oil refining and electric power generation industries [31]. The Red Cross area also shows a high soil and water pollution ranking as one of the most polluted areas in Salamanca, Mexico (See Figure 2). Figure 3 shows the Red Cross Station location and the TPP. The tract and dispersion are indicated by the redline at which meteorological data and SO<sub>2</sub> concentrations were obtained [32].



**Figure 2.** (a) High soil and water pollution of the Salamanca entity, (b), Guanajuato location in the Mexican Republic Map (c) Salamanca, the most Polluted entity area in Guanajuato. Source: Adapted from Google Earth (2020) [32].



**Figure 3.** Tract and dispersion of SO<sub>2</sub> are indicated in the closest neighborhood on Salamanca's Map from the TTP emission source monitored by the Red Cross station. Source: Adapted from Google Earth (2020) [32].

## 4. The Gaussian Model

Based on the assumption of the flux of matter per unit area and per unit time, Fick's first law for molecular diffusion is used as follows:

$$J = -K \frac{\partial C}{\partial x} \tag{1}$$

where:

J = Mass flux of the pollutant (ML<sup>-2</sup> T<sup>-1</sup>).

 $\partial C$  = Concentration variation of the pollutant (ML<sup>-3</sup>).

 $\partial x$  = Distance variation (L).

K = diffusion coefficient (L<sup>2</sup> T<sup>-1</sup>). The material balance assumes the following:

$$\frac{\partial C}{\partial t} = \frac{\left[ (flux)_x - (flux)_{x+\Delta x} \right]}{\Delta x} = K \frac{\partial^2 C}{\partial x^2}$$
(2)

The solution of this one-dimensional equation is:

$$C(x,t) = \frac{M_o}{2(\pi tK)^{1/2}} e^{\left[-\left(\frac{1}{4t}\right)\left(\frac{x^2}{K}\right)\right]}$$
(3)

where  $M_0$  is the mass deposited at t = 0. The following formula is used:

$$\sigma_x = \left(2Kt\right)^{1/2} \tag{4}$$

where  $\sigma_x$  = turbulent dispersion coefficient (L).

It follows that:

$$C(x) = \frac{M_o}{(2\pi)^{1/2} \sigma_x} e^{-(\frac{x^2}{2\sigma_x^2})}$$
(5)

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In this one-dimensional equation, the concentration C is in units of mass per unit length (M/L).

For three-dimensional flow, the relationship must be extended by defining the turbulent dispersion coefficients  $\sigma_x$ ,  $\sigma_y$ , and  $\sigma_z$  for the x, y, and z directions, respectively, such that:

$$C(x,y,z) = \frac{M_0}{(2\pi)^{3/2} \sigma_x \sigma_y \sigma_z} e^{-(\frac{x^2}{2\sigma_x^2})} e^{-(\frac{x^2}{2\sigma_y^2})} e^{-(\frac{x^2}{2\sigma_z^2})}$$
(6)

Equation (6) solves the emission of a point source and allows the pollutant mass to be identified using Gaussian distribution equations. When it comes to an industrial chimney discharge, the phenomenon is studied in two dimensions. When dispersion is placed on the x axis, this can be ignored, since on this axis, only transport of pollutants due to the effects of wind occurs, although it would be interesting to study the dynamics of atmospheric turbulence in the *y* and *z* directions. For a 2-dimensional scattering processes involving the horizontal direction (y axis) and vertical direction (z axis), the equation is reduced to:

$$C(y,z) = \frac{M_o}{2 \pi \sigma_y \sigma_z} e^{-(\frac{y^2}{2\sigma_x^2})} e^{-(\frac{z^2}{2\sigma_z^2})}$$
(7)

Along the horizontal axis (y axis), mass is assumed to be unproblematic for particle deposition, but on the vertical axis (z axis), it is deposited at a height H called the effective emission height; therefore, an axis shift must be performed using the following equation:

$$H \rightarrow z - H$$
 (8)

Furthermore:

$$C(y,z) = \frac{M_o}{2 \pi \sigma_y \sigma_z} e^{-\frac{y^2}{2\sigma_x^2}} e^{-\frac{(z-H)^2}{2\sigma_z^2}}$$
(9)

The mass  $M_0$  can be determined by the relationship:

$$M_o = \frac{Q}{U} \tag{10}$$

where:

Q = emission rate of the gaseous pollutant (MT<sup>-1</sup>).

U = average wind speed (LT<sup>-1</sup>).

After making the substitution, the above equation results in a mathematical expression of the two-dimensional Gaussian model:

$$c(y,z,H) = \frac{Q}{2\pi U \sigma_y \sigma_z} exp\left[-\frac{y^2}{2\sigma_y^2} + \frac{(z-H)^2}{2\sigma_z^2}\right]$$
(11)

The concentration at ground level is of significant interest in this study, so it is considered at y = 0 and z = 0. Therefore, Equation (11) is expressed as:

$$c(x,0,0,H) = \frac{Q}{2\pi U \sigma_y \sigma_z} exp\left[-\frac{H^2}{2\sigma_z^2}\right]$$
(12)

For the solution of Equation (12), some considerations were made: Theoretical considerations.

- 1. The stack is a point source of emission.
- 2. The terrain where the dispersion of pollutants takes place is flat.
- 3. The pollutant flow is incompressible.
- 4. Turbulent flows are related to the gradients of the average concentrations.
- 5. Pollutant diffusion is passive.
- 6. Longitudinal diffusion and molecular diffusion are minimal and can be neglected.
- 7. Both lateral and vertical wind speeds are considered to be zero.
- 8. The location of the emission chimney, EC, stack is rural, according to its geographic coordinates and the shortest distance to the population.
- 9. It is assumed that the transport of pollutants occurs in a straight line, instantaneously, in the wind direction.

Some considerations were also made to obtain the dispersion coefficients ( $\sigma_y$  and  $\sigma_z$ ). Table 3 shows that  $\sigma_y$  and  $\sigma_z$  are a function of the atmospheric stability category (ASC), and the distance on the x-axis, measured from the base of the stack in the direction of the plume [29].

ASC	$\sigma_y$	$\sigma_z$
A	$0.22x (1 + 0.0001x)^{-1/2}$	0.20x
В	$0.16x (1 + 0.0001x)^{-1/2}$	0.12x
С	$0.11x (1 + 0.0001x)^{-1/2}$	$0.08x (1 + 0.0002x)^{-1/2}$
D	$0.08x (1 + 0.0001x)^{-1/2}$	$0.06x (1 + 0.0015x)^{-1/2}$
Е	$0.06x (1 + 0.0001x)^{-1/2}$	$0.03x (1 + 0.003x)^{-1}$
F	$0.04x (1 + 0.0001x)^{-1/2}$	$0.016x (1 + 0.0003x)^{-1}$

Table 3. Pasquill-Gifford dispersion coefficients of Briggs's interpretation.

Source: Data from [29].

The Gaussian distribution indicates y = 0, where the pollutant is most concentrated is in the transverse *y* coordinate, since it coincides with the wind direction or studies related to the dispersion of stationary sources (see Figure 4).



**Figure 4.** Dispersion coefficients. (a) Top view of dispersion  $\sigma_y$ , (b) dispersion z exe,  $\sigma_z$ . Source: own elaboration and adapted from the two-dimensional Gaussian model [29].

There are two ways in which the dispersion coefficient can increase, which mathematically represents the width of the Gaussian bell, which means that the concentration of the pollutant decreases due to atmospheric dilution: when the x-distance, measured from the foot of the chimney increases, and when the atmospheric instability increases. This means that turbulence facilitates the dispersion of pollutants. So, at night and in rural areas, the dispersion coefficients are smaller [21].

Wind speed considerations:

For heights less than 10 m, wind speed is affected by friction and must be corrected by the following equation:

$$U_z = U_{10} \left(\frac{h}{10}\right)^p \tag{13}$$

where:

 $U_z$  = wind speed at the height of the emitting source (m/s).

 $U_{10}$  = wind speed at the 10 m height (m/s).

h = height of the emitting source (m).

p = atmospheric exponential coefficient of the urban or rural environment according to the stability category (see Table 4).

Table 4. Correction for wind speed.

ASC	Coeffic	cient p
ASC	Urban	Rural
A	0.15	0.07
В	0.15	0.07
С	0.2	0.1
D	0.25	0.15
E	0.3	0.35
F	0.3	0.35

Source: Data from [21].

Considerations for the effective height *H*:

To obtain the effective emission height (*H*), it is necessary to consider the plume height ( $\Delta h$ ) plus the stack height (*h*) as indicated in the following equation:

$$H = h + \Delta h \tag{14}$$

The calculation of  $\Delta h$  requires other atmospheric parameters (temperature and pressure) and stack data, such as the diameter and pollutant exit velocity.  $\Delta h$  can be obtained using Holland's equation [33]:

$$\Delta h = \frac{DV_s}{U} \left( 1.5 + 2.68 \times 10^{-3} \ PD \frac{T_s - T_a}{T_s} \right)$$
(15)

where:

 $V_s$  = pollutant exit velocity (m/s).

D = diameter of the chimney (m).

P =atmospheric pressure (mbar).

 $T_s = SO_2$  outlet temperature (°K).

 $T_a$  = atmospheric temperature (°K).

 $2.68 \times 10^{-3} = \text{constant} (1/\text{m mbar}).$ 

Plume height correction ( $\Delta h$ ) is achieved using the Paquill–Gifford–Tunner factor shown in Table 5.

Table 5. Factors of plume elevation.

<b>Correction Factor</b>	ASC
1.15	А
1.15	В
1.1	С
1	D
0.85	Е
0.85	F

Source: Data from [21].

### 5. The Origin of the Data

The statistical average was obtained from Red Cross station environmental data historical values of the variables, temperature, and atmospheric pressure at the Secretary of Environment and Territorial Planning of Guanajuato official site in 2017 [34]. Validation of the results was performed using the four thermal power plant stacks. The SO<sub>2</sub> concentrations, technical data regarding the dimensions, and pollutant emissions were obtained from the same source [14].

#### 6. Meteorological Data and SO<sub>2</sub> Concentration Data

The historical Red Cross Station quality data were analyzed [34] to calculate the monthly and annual average pressure, temperature, wind speed, and direction. Figure 5a shows the monthly average 24 h pressure, which varies between 621.3 and 624.8 mmHg, while the temperature under the same conditions ranges from 17.8 to 22.5 °C in 2017. In Figure 5b, the monthly average SO<sub>2</sub> concentrations range between 2.64 and 14.96  $\mu$ g/m<sup>3</sup>. Meanwhile, the maximum and minimum values were recorded in the warm and cold seasons, respectively.



**Figure 5.** (a) 24 h average atmospheric pressure and room temperature and (b) 24 h  $SO_2$  average concentration. Source: own elaboration.

The predominant wind direction through the WRPLOT View by Lakes Environmental Software (Waterloo, Ontario, Canada) is in a westerly direction, right at the Red Cross station (RCS). The monthly average wind speed varies between 0.45 and 8.34 m/s, according to the historical data reported by the official site, as shown in Figure 6.



Figure 6. Wind at the RC station Google Earth. Source: Adapted from Google Earth 2020.

Figure 7 shows the meteorological conditions (room temperature, barometric pressure, wind speed, time of day, and atmospheric stability conditions) that were considered in the modeling approach.

The daytime and nighttime dispersion categories of Pasquill–Gifford–Turner were using to establish the modeling sceneries, as shown in Table 6. The SO<sub>2</sub> concentrations and meteorological conditions, including room temperature and wind speed, were obtained from the data already mentioned in this section.



Figure 7. Modeling sceneries.

Table 6. Pasquill-Gifford-Turner dispersion categories.

V(m/s) (10 m)	Suns	troke during the	e Day	Cloud Cover Overnight		
v (m/s) (10 m)	Strong	Moderate	Little	Few Clouds	Without Clouds	
2	А	A–B	В			
2–3	A–B	В	С	E	F	
3–5	В	B–C	С	D	E	
5–6	С	C–D	D	D	D	
6	С	D	D	D	D	

Source: Data from Zambrano (2018, p. 22). Note: F = strong, M = moderate, and L = mild.

The Gaussian model assumes that meteorological conditions do not change over a considerable period of time. So, the model scenery approaches a set of conditions with an average minimum and maximum annual wind speed of 2.4 and 8.4 m/s, respectively, in Salamanca city.

Regarding temperature, the monthly average during the day and night was 24.2 and 19.2 °C, respectively. Moreover, three types of solar irradiation were contemplated: strong, moderate, and light. The Pasquill–Gifford–Turner ASCs were A, B, and C, respectively. During the night (cloudy and cloudless), the ASC scenarios were E and F. For a maximum average wind speed of 8.4 m/s, three types solar irradiation were considered based on the following Pasquill–Gifford–Turner ASCs: C and D. During the night (cloudy and cloudless), the only anticipated ASC scenario was D. Based on the total emissions obtained, the sum of the four stacks' SO<sub>2</sub> concentration was assumed to be representative of an annual cycle (see Table 7).

Table 8 shows the modeling variables and technical  $SO_2$  emission and design data for the four stacks, which considered the information from the application of the model.

Figure	Scenario	V (m/s)	T (°C)	ASC	Schedule	Chimney
8	1	2.4	24.2	А	day	1, 2, 3 and 4
9	2	2.4	24.2	В	day	1, 2, 3 and 4
10	3	2.4	24.2	С	day	1, 2, 3 and 4
11	6	8.4	24.2	С	day	1, 2, 3 and 4
12	7	8.4	24.2	D	day	1, 2, 3 and 4
13	8	8.4	19.5	D	night	1, 2, 3 and 4

Table 7. Scenarios and conditions of the modeling variables according to ASC.

Table 8. Stack data, emissions, and geographic and meteorological conditions.

Davamatar	Symbols	Units	5	Smokestack	s
raiantetei			1	2 and 3	4
Emission rate	Q	g/s	871	871	871
Coefficient of dispersion in the Y axis <sup>a</sup>	$\sigma_y$				
Coefficient of dispersion in the Z axis <sup>a</sup>	$\sigma_z$				
Wind speed *	U	m/s	2.4	2.4	2.4
Atmospheric temperature *	Ta	°K	295	295	295
Atmospheric pressure *	Р	mbar	831	831	831
Pollutant outlet temperature *	Ts	°K	438.5	432.1	431
Pollutant outlet velocity *	$v_s$	m/s	22.8	29.1	28.5
Smokestacks diameter	D	m	4.5	3.9	3.4
Smokestacks height	h	m	64.6	51.2	49.7
Boom lift height <sup>a</sup>	$\Delta H$	m			
Effective height <sup>a</sup>	Н	m			
Concentration **a	С	g/m <sup>3</sup>			

\* Meteorological variables; \*\* ASS: B, D y F; <sup>a</sup> is calculate.

#### 7. Results

In agreement with the literature results [26,27,35], the importance of health risk management in highly industrialized cities is highlighted in in all models. The variation in the SO<sub>2</sub> concentration from the base of the stacks up to 5000 m shows that at larger distances, SO<sub>2</sub> pollution is reduced by dispersion. These results are demonstrated by the SO<sub>2</sub> concentrations in the Gaussian model for the proposed scenarios.

The modeling of scenario 1 (Figure 8a) shows ASC A with strong and moderate irradiation at a wind speed of 2.4 m/s during the day in the 4 stacks: stack 1 recorded an SO<sub>2</sub> concentration of 490  $\mu$ g/m<sup>3</sup> at 1000 m while stacks 2 and 3, with the same dimensions, reached a maximum value of 551  $\mu$ g/m<sup>3</sup> at 900 m. Finally, at 700 m, stack 4 reached a concentration of 355  $\mu$ g/m<sup>3</sup>. With respect to the scenario modeling 2 with ASC B, the maximum SO<sub>2</sub> concentrations ( $\mu$ g/m<sup>3</sup>) for stacks 2 and 3, 1, and 4 were 467  $\mu$ g/m<sup>3</sup> at 1500 m, 413  $\mu$ g/m<sup>3</sup> at 1500 m, and 301  $\mu$ g/m<sup>3</sup> at 1300 m (see Figure 8b), respectively. The results were above the limits established in the Official Mexican Standard, 2010 (NOM-DOF 2010).

Figure 9a shows the results of the modeling scenario 3, ASC B, and the SO<sub>2</sub> concentrations for stacks 2 and 3, 1, and 4 were 409  $\mu$ g/m<sup>3</sup> at 3000 m, 368  $\mu$ g/m<sup>3</sup> at 3000 m, and 280  $\mu$ g/m<sup>3</sup> at 2000 m, respectively, which are slightly below the maximum limits established in the Official Mexican Standard, 2010 (Official Mexican Norm Published officially in 2010) NOM-DOF 2010. For sceneries 4 and 5, ASC E and F, the SO<sub>2</sub> concentrations, under partly cloudy and clear sky conditions and a relatively calm wind speed (2.4 m/s), were not detected in the Gaussian model due to an inherent flaw [29]. However, the detection of these concentrations using adequate models that precisely coincide with the worst conditions, which present greater risk, is relevant [22]. For scenario 6, ASC C, a wind speed of 8.4 m/s during the day was observed, and the maximum SO<sub>2</sub> concentrations for stacks 2 and 3, 1, and 4 were 659  $\mu$ g/m<sup>3</sup> at 1000 m, 506  $\mu$ g/m<sup>3</sup> at 1100 m, and 380  $\mu$ g/m<sup>3</sup> at 900 m, respectively. These results are higher than the limits established in the Official Mexican Standard, NOM-022-SSA1-2010 (see Figure 9b).



Figure 8. (a) Scenario 1 and (b) scenario 2. Source: Author's elaboration.



Figure 9. (a) Scenery 3 and (b) scenery 4. Source: Author's elaboration.

Figure 10a shows the results of scenario 7, ASC D, for a daytime wind speed of 8.4 m/s. The SO<sub>2</sub> concentrations ( $\mu$ g/m<sup>3</sup>) for stacks 2 and 3, 1, and 4were 413 at 2000 m, 285 at 3000 m, and 242 at 1500 m, respectively. Finally, the modeling results of scenario 8, which corresponds to ASC D, at a velocity of 8.4 m/s during the night yielded the following SO<sub>2</sub> concentrations ( $\mu$ g/m<sup>3</sup>) for stacks 2 and 3, 1, and 4: 412 at 2000 m, 285 at 3000 m, and 280 at 3000 m, respectively (see Figure 10b). Some authors in the literature have reported a decrease in the maximum concentrations of gaseous pollutants as the atmospheric instability decreases [29,36].

Table 9 shows the profile of the maximum concentrations in the Gaussian modeling sceneries. The distances in the direction of the pollution plume at which the maximum  $SO_2$  concentrations were reached are reported.

Regarding the wind trajectory, in all stacks, the emissions behavior exceeded the standard value (288  $\mu$ g/m<sup>3</sup>) and was decreased by 12.15 %, 35.7 %, and 68.4 % at an average distance of 1,800 m, respectively. Larger distance values were found between 700 and 2000 m. Meanwhile, lower distance values were found at 3000 m. Finally, stacks 2 and 3 exceeded the emissions, reaching 485  $\mu$ g/m<sup>3</sup> at an average distance of 1933 m.



Figure 10. (a) Scenary 7 and (b) scenery 8. Source: Author's own elaboration.

Table 9. Profile of the maximum SO<sub>2</sub> concentrations at a distance (d) from the emission sources.

Conditions				Distance (m) and Concentration (C) by Smokestack						
Setting	V (m/s)	T (°C)	ASC	Schedule	d (m)	2 and 3	d (m)	1	d (m)	4
1	2.4	24.2	А	Day	900	551	1000	490	700	355
2	2.4	24.2	В	Day	1500	467	1500	413	1300	301
3	2.4	24.2	С	Day	3000	409	2000	368	3000	280
4	2.4	19.5	Е	Night						
5	2.4	19.5	F	Night						
6	8.4	24.2	С	Day	1000	659	1100	506	900	380
7	8.4	24.2	D	Day	2000	413	3000	285	1500	242
8	8.4	19.5	D	Night	2000	412	3000	285	3000	280

The vertical emission length did not represent a risk to the city due to the complete profile of the emission plume, which tended to descend as the horizontal distance increased. Overall, the Gaussian model showed that the average maximum  $SO_2$  concentration is 399 µg/m<sup>3</sup>, which is above the standard value (indicated by the maximum limits established in the NOM-022-SSA-010), at a distance of 1800 m. This considers the Red Cross (RC) monitoring station's location at 3000 m. The best  $SO_2$  dispersion was obtained in scenario 8, corresponding to nighttime and at a relatively high speed 8.4 m/s and a concentration of 280 µg/m<sup>3</sup>, which are optimal values for a geographical site where, historically, wind conditions are calm. Concerning daytime, the best dispersion occurred in scenario 7 with high wind speed and strong solar irradiation. These results are similar to previously reported results [21,35]. Validation was performed based on the relative error in the SO<sub>2</sub> emissions as shown by Equation 16:

$$\% E_r = \frac{C_m - C_e}{C_m} (100)$$
 (16)

where:

 $E_r$  = relative error.

 $C_m$  = station concentration value (µg/m<sup>3</sup>).

 $C_e$  = estimated value (µg/m<sup>3</sup>).

The estimated value obtained for the stacks with the concentrations added at 3000 m was 1198  $\mu$ g/m<sup>3</sup>, which was located at the RC station point. TPP emissions corresponded to 4.1% of the total SO<sub>2</sub> emissions in the Salamanca municipality in 2017 [34]. Hence, the total emissions were 29,146  $\mu$ g/m<sup>3</sup>. On the other hand, the measured value reported by the RC station was 34,191  $\mu$ g/m<sup>3</sup> and the absolute error was 14.7%. The model predicted more accurate values for the daytime dispersion phenomenon at moderate velocities between 2 to 3 m/s. This type of validation could be related to the pollutant stacks considered [37].

## 8. Discussion

Modeling is a valuable engineering tool for technology development for atmospheric monitoring, and its estimation. Its application to emission stacks allows for real-time air quality monitoring and control. Medium-term projections provide information for management evaluation strategies, which aim to comply with the national standards established by WHO. The maximum SO<sub>2</sub> concentration profile results from the model revealed that during the day and night, the emission focus was the four chimneys of the Salamanca TPP where the concentrations reached residential areas. When the stability decreased in ASC A, B, and C, the maximum SO<sub>2</sub> concentration also decreased.

The Gaussian model applied yielded an error close to 15%, representing a valuable mathematical tool for the generation of scientific evidence of the complex phenomenon of atmospheric pollutant dispersion to ground level. The model handles multiple variables (geographical, meteorological, such as temperature and atmospheric pressure, wind speed and direction) and design characteristics of the chimneys (height and diameter, and the type of fuels used on an industrial scale). Using this modeling process, some theoretical considerations, and others specific to the physical area where the study was carried out, allowed us to show the  $SO_2$  dispersion scenarios.

The findings show that, in a terrain of simple roughness, low wind speed, and ambient temperatures that are not extreme, as is the case of Salamanca city, SO<sub>2</sub> dispersion in the horizontal path direction along the Gaussian plume exceeds the concentrations allowed during the day. A comparison with the calculation of the atmospheric dispersion coefficients employed in other mathematical formulations, such as Turner, Hosker, Mc-Mullen, or the Industrial Source Complex Short Term, ISCST models, CALPUFF model (California integrated Lagrangian PUFF modeling system), is suggested. It is important to broaden the spectrum to study three dimensions to completely analyze the atmospheric dispersion phenomenon. This information could be useful for the activation of transversal projects of a technical or epidemiological nature, using cleaner fuels, such as natural gas, to reduce SO<sub>2</sub> and PM<sub>10</sub> emissions (pollutants that trigger the activation of environmental pre-contingencies) from the effluents of TC chimneys, thus reducing health risks in the population.

#### 9. Conclusions

The production of electricity from fuel oil showed severe implications on climate change and the health of inhabitants due to SO<sub>2</sub> emissions, which require greater vigilance. The atmospheric monitoring station in Salamanca city, Red Cross (RC), found that meteorological conditions do not change over a considerable period of time and that the model scenery is related to gradients, such as the wind speed, dispersion, and the concentration of particulate material, such as SO<sub>2</sub>, which are related to the atmospheric stability category. The maximum average SO<sub>2</sub> concentration was 399  $\mu$ g/m<sup>3</sup> at an average distance of 1800 m. In the scenarios comparison, scenery 8 showed better results. The nocturnal dispersion showed a maximum wind speed of 8.4 m/s and an SO<sub>2</sub> concentration of 280  $\mu$ g/m<sup>3</sup> for stack 4, which is an atypical situation due to the geography of the city. From the validation process, a relative error of 14.7% was obtained, which indicates the reliability of the applied Gaussian model. Regarding the mathematical solution of the model, this represents a reliable and low-cost tool that can help improve air quality management, the location or relocation of atmospheric monitoring stations, and migration from the use of fossil fuels to environmentally friendly fuels.

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