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Harvesting *Scenedesmus obliquus* via Flocculation of *Moringa oleifera* Seed Extract from Urban Wastewater: Proposal for the Integrated Use of Oil and Flocculant

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Abstract: The objectives this study were to examine the integrated use of oil-coagulant for the direct extraction of coagulant from *Moringa oleifera* (MO) with 5% and 10% (NH₄)₂SO₄ extractor solution to harvest *Scenedesmus obliquus* cultivated in urban wastewater and to analyze the oil extracted from MO and *S. obliquus*. An average content of 0.47 g of coagulant and 0.5 g of oil per gram of MO was obtained. Highly efficient algal harvest, 80.33% and 72.13%, was achieved at a dose of 0.38 g L⁻¹ and pH 8–9 for 5% and 10% extractor solutions, respectively. For values above pH 9, the harvest efficiency decreases, producing a whitish water with 10% (NH₄)₂SO₄ solution. The oil profile (MO and *S. obliquus*) showed contents of SFA of 36.24–36.54%, monounsaturated fatty acids of 32.78–36.13%, and polyunsaturated fatty acids of 27.63–30.67%. The biodiesel obtained by *S. obliquus* and MO has poor cold flow properties, indicating possible applications limited to warm climates. For both biodiesels, good fuel ignition was observed according to the high cetane number and positive correlation with SFA and negative correlation with the degree of saturation. This supports the use of MO as a potentially harmless bioflocculant for microalgal harvest in wastewater, contributing to its treatment, and a possible source of low-cost biodiesel.

Keywords: coagulation-flocculation; harvest microalgal; *Moringa oleifera*; *Scenedesmus obliquus*; biodiesel quality

1. Introduction

Bodies of water are constantly exposed to various concentrations of pathogenic bacteria, nutrients, organic matter, and heavy metals, occasionally reaching dangerous levels [1,2]. Conventional methods for wastewater treatment are expensive and sometimes inefficient depending on the technology used and their type of maintenance. Wastewater is usually discharged into natural receiving bodies of water but does not contaminate ecosystems or threaten human health with proper treatment. Although various technologies are available for the treatment of wastewater, the use of photosynthetic microorganisms has received attention as an alternative for the removal of nutrients; for this reason, researchers have concluded that the cultivation of microalgae in wastewater provides dual benefits:

the efficient removal of nutrients and the production of algal biomass that can be used as raw material for the extraction of high value chemicals and biofuel synthesis (bioethanol and biodiesel).

One of the major practical limitations of wastewater treatment using photosynthetic microorganisms is harvesting the algal biomass from the treated effluent. Some methods, such as centrifugation, flocculation, chemical coagulation, electrolytic process, gravity sedimentation, filtration and screening, flotation, dissolved air flotation, dispersed air flotation, electrophoresis techniques, and immobilized cells, are expensive given the maintenance and energy requirements [3–6], through which harvesting could only be justified in cases where high-cost products are fabricated, such as drug precursors and materials for pharmaceutical purposes [7]. This means that operating costs should be decreased drastically to ensure that production and commercialization become feasible.

Physicochemical processes are widely adopted to treat wastewater effluents, including membrane filtration, ion exchange, advanced oxidation, adsorption, and coagulation–flocculation [8–10]. Coagulation–flocculation is particularly attractive among the processes due to its low cost, simple operation, high efficiency biomass recovery, and improvement of the effluent's quality [11]. Selecting the coagulant influences the recovery efficiency of algal biomass; the coagulant's use should not contaminate and affect the biomass's quality, since this would incur additional costs for the biomass's purification. The synthesis of coagulants includes inorganic and organic coagulants, which are widely used for the treatment of wastewater. However, studies suggest that some of these coagulants have negative effects, such as the aluminum coagulant causing Alzheimer's disease and the acrylamide monomer in polyacrylamide also being neurotoxic to humans [12–14]. Therefore, the demand is increasing for the use of coagulants with higher efficiency that are safe for both the environment and human health.

Natural coagulants extracted from plants such as *Moringa oleifera* seed, *Jatropha curcas*, copra, and cactus have shown promise as abundant raw materials for obtaining biodegradable organic coagulants with low toxicity [15]. As a coagulant, *M. oleifera* seeds have been recognized as one of the best natural products for wastewater treatment. Studies have reported that the seeds can be used to remove pollutants including turbidity, heavy metals, *Escherichia coli* bacteria, algae, and water surfactants [2,6,10], which is attributed to the cationic protein contained in *M. oleifera* seeds as an active bio-coagulating component for the treatment of wastewater. The seeds have potential as biofloculants in the microalgae biomass separation process and harvesting [16]. The objective of this study was to explore the potential of the oil and biocoagulant–floculant of *M. oleifera* seed in microalgae cultures in wastewater and to evaluate the possible effects of floculant contamination on the biodiesel quality obtained from the synthesis of algal fatty acids.

2. Materials and Methods

2.1. Seed Preparation *Moringa Oleifera* (MO)

The MO seeds were obtained from trees that grow in the region of Ciudad del Carmen, Campeche, Mexico. The dried pods were collected and cleaned manually, leaving the seeds free from rind. The MO seeds were dried in an oven at 60 °C for 24 h and then ground and sieved in a stainless steel sieve (600 µm) until a homogeneous fine powder was produced. For conservation, MO powder was stored in moisture- and light-free containers to prevent oxidation and the degradation of its active properties.

2.2. Oil Extraction

The oil extraction was performed according to Sato and Murata [17] and Canedo-Lopez et al. [18]. Six samples in a triplicate of different quantities (P_1) of MO powder (1, 2, 4, 6, 8, and 10 g) were used for the oil extraction. For each sample, 50 mL of chloroform–methanol solution (2:1 v/v) was added, then the MO and solvent mixture was placed in ultrasonic equipment (70 Hz) for 1 h at 4 °C. The samples were centrifuged (4500 rpm, 25 min) and the solvent–oil supernatant was evaporated to concentrate the oil for subsequent transesterification prior to the identification of lipids. The oil-free MO extract

was oven-dried (60 °C) up to a constant weight (P_2) for 24 h. The weight difference between P_1 and P_2 represents the extracted oil content (g).

2.3. Removal of One-Step Flocculant

To obtain an inexpensive coagulant and for practical purposes, a simple one-step extraction methodology was used as it is feasible to use on larger scales, where the coagulant-flocculant efficiency could be conserved in microalgae cultures in wastewater. The procedure consisted in extracting coagulant protein from the oil-free MO extract. For the MO sample, a 50 mL of 5% and 10% $(\text{NH}_4)_2\text{SO}_4$ solution was added. The samples were placed in ultrasonic equipment (70 Hz) for 15 min at 4 °C, and let to stand for 24 h in refrigeration and darkness. After this time, the samples were centrifuged (4500 rpm) for 15 min and the supernatant containing the coagulant was separated and kept under refrigeration in the dark for subsequent coagulation–flocculation efficiency tests using the jar test equipment in *Scenedesmus obliquus* cultures from urban wastewater and urban wastewater only. The extraction of coagulant-free MO was dried in an oven (60 °C) up to a constant weight (P_3) for 24 h, with the difference in weight between P_2 and P_3 was used to determine the content of coagulant (g).

2.4. Cultivation of the Microalga *Scenedesmus Obliquus*

S. obliquus microalga was selected for its ability to grow in urban wastewater and efficiently remove nitrogen and phosphorus. The composition of the equivalent culture medium (CME) for the acclimatization of *S. obliquus* was designed according to the main characteristics of a primary treatment effluent [4], with the addition of trace metals and vitamins similar for f/2 medium [19]. The culture conditions for an initial cellular density of 2×10^6 cells mL^{-1} were 28 ± 1 °C at a light intensity of $100 \mu\text{E m}^{-2} \text{s}^{-1}$ using light-white fluorescent lamps and $0.4 \text{ L L}^{-1} \text{min}^{-1}$ aeration. For the analysis of coagulation–flocculation efficiency, the *S. obliquus* microalgae was cultivated in six cylindrical bioreactors composed of 2 L transparent polyethylene terephthalate (PETE) containing CME in triplicate, pre-washed with a chlorine solution (0.5%) to prevent bacterial contamination. The two-stage method was used to increase the accumulation of lipids in all cultures. The procedure consisted of installing reactors of culture with an initial volume of 1 L with half residual water enriched with nitrogen ($90 \text{ mg N-NH}_4 \text{ L}^{-1}$), with the cultures diluted at the end of the exponential phase by adding fresh medium (1 L) until a concentration of $10 \text{ mg N-NH}_4 \text{ L}^{-1}$ was reached.

For the analysis of the coagulation efficiency in a domestic effluent, samples were collected from the discharge of aerobic treatment plants (Table 1). The samples were homogenized to obtain a representative sample of urban wastewater from the treatment plants in the municipality of the Ciudad del Carmen, Campeche; Mexico.

2.5. Experimental Design: Jar Test

A standard jar test was used to explore the coagulation–flocculation efficiency. A series of six 1.5 L reactors were installed containing cultures of *S. obliquus* in urban wastewater and another series with only urban wastewater. To determine the optimal dose, the flocculant extracted from the MO was added in each of the reactors and mixed rapidly (120 rpm) for 30 s, followed by a lens mixture (40 rpm) for 30 min [10,20]. The mixture was allowed to settle for 1 h and water samples were collected to determine turbidity. The sediment microalgae were collected and centrifuged (4000 rpm for 15 min), eliminating the largest amount of water for subsequent lyophilization and lipid extraction. The percentage of removal (R) for both treatments was calculated with the following equation:

$$R = \frac{C_o - C_f}{C_o} * 100$$

where C_o and C_f are the initial and final turbidity, respectively.

Table 1. Chemical parameters determined for wastewater effluent of treatment plants (WPT). The results represent average values (samples in triplicate) and standard deviation (\pm SD).

Parameter	Units	Effluent Characteristics		
		WPT ₁	WPT ₂	WPT ₃
Temperature	°C	26.3 \pm 0.2	27.0 \pm 0.1	27.6 \pm 0.01
pH		7.96	7.47	7.10
Total phosphorus	mg L ⁻¹	19.64 \pm 0.1	3.75 \pm 0.2	4.22 \pm 0.02
Total nitrogen	mg L ⁻¹	99.13 \pm 0.02	18.64 \pm 0.1	3.10 \pm 0.1
N-NH ₄	mg L ⁻¹	90.75 \pm 0.03	17.06 \pm 0.02	2.84 \pm 0.02
N-NO ₃	mg L ⁻¹	8.29 \pm 0.01	1.81 \pm 0.01	0.32 \pm 0.03
N-NO ₂	mg L ⁻¹	0.08 \pm 0.1	0.013 \pm 0.2	0.002 \pm 0.2
Rate N/P		5.04	4.97	0.73
Fats and oil	mg L ⁻¹	20.26 \pm 1.2	8.03 \pm 2.2	10.75 \pm 1.8
BOD	mg L ⁻¹	212 \pm 0.8	28 \pm 1.2	43 \pm 0.5
SST	mg L ⁻¹	117 \pm 0.5	27 \pm 0.2	40 \pm 0.3
Turbidity	NTU	981	830	633

Note: BOD: Biochemical Oxygen Demand; SST: Total Suspended Solids; NTU: Nephelometric Turbidity Units.

2.6. Fatty Acid Methyl Esters (FAME) Profile

The biomass recovered from the jar test was frozen at -4.0 °C for 48 h, and then lyophilized for 3 days; the resulting dry biomass was stored at 0 °C. Total lipids were extracted following the dry extraction procedure described by Canedo-Lopez et al. [18]. The transesterification of fatty acids for the algal biomass and MO were according to the methods reported by Sato and Murata [17]. The FAME profiles were determined using a gas chromatographer (GC) (Agilent Technology 7890, CA, USA). One microliter of the FAME-hexane solution was injected into the GC equipped with a flame ionization detector (FID) and DB-23 column (60 m length, 0.32 mm internal diameter, 0.25 μ m thick); helium was the carrier gas. The injector and detector temperature was 250 °C. The temperature program was: 120 °C for 5 min; 10 °C min^{-1} increases until reaching 180 °C for 30 min; 10 °C min^{-1} increases until reaching 210 °C for 21 min. A calibration curve was prepared for all FAMES by injecting known concentrations of an external standard mixture containing 37 FAMES (Supelco, Bellefonte, PA, USA); the correlation coefficient was equal to or greater than 95% in all cases.

2.7. Biodiesel Fuel Property Estimates

The biodiesel quality parameters obtained from *S. obliquus* and MO were estimated as described by Vidyashankar et al. [21] and Guldhe et al. [22].

The saponification value (SV), cetane number (CN), iodine value (IV), long chain saturated factor (LCSF), and cold filter plugging point (CFPP) were estimated for the fatty acid composition of the microalgae and MO as described by Vidyashankar et al. [21] and Guldhe et al. [22]:

$$SV = \sum \frac{560N}{M}, \quad (1)$$

$$IV = \sum \frac{254DN}{M}, \quad (2)$$

$$CN = 46.3 + \frac{5458}{SV} - 0.225 IV, \quad (3)$$

$$LCSF = [0.1 C16(\text{wt } \%) + 0.5 C18(\text{wt } \% + 1. C20(\text{wt } \%) + 1.5 C22(\text{wt } \%) + 2. C24(\text{wt } \%)], \quad (4)$$

$$CFPP = (3.1417 * LCSF) - 16.477, \quad (5)$$

where SV , CN , IV , $LCSF$, and $CFPP$ are the saponification value, cetane number, iodine value, long chain saturated factor and cold filter plugging point, respectively; and D , M , and N denote the number of double bonds, molecular mass, and percent mass fraction of each fatty acid component, respectively.

$$DU = MUFA + (2 * PUFA) \quad (6)$$

$$\text{Oxidative stability (OS)} = -(0.0384 * DU) + 7.77 \quad (7)$$

where DU is the amount of unsaturated fatty acid (MUFA) and polyunsaturated fatty acid (PUFA), calculated from the fatty acid profile [22,23]. The properties of synthesized biodiesel were compared with the specifications provided by ASTM 6751 and EN14214 standards.

2.8. Statistical Analysis

An analysis of variance (ANOVA, $P \leq 0.05$) was applied to evaluate the optimum dose and pH in the coagulation–flocculation potential of the *M. oleifera* seed on *S. obliquus* cultures in urban wastewater. The effect of the coagulant in the fatty acid profiles of the algal biomass harvested and synthesis of biodiesel was also evaluated. Tukey's test of honestly significant difference (HSD) was applied when results exhibited significant differences.

3. Results and Discussion

Our study of the integrated use of MO seed included an analysis of the potential of extracted oil and bioflocculating–coagulating activity (Figure 1). The results showed a positive correlation (correlation coefficient (R) = 0.94) between the oil content and the amount of MO (Figure 2) suggesting that for each gram of the *M. oleifera* seed, approximately 0.5 g oil can be obtained (50%, w/w) (Equation (8)).

With this method, MO shows potential as a raw material source of low-cost energy according to the content and characteristics of the oil, with the additional advantage of having potential as a bioflocculant for the recovery of algal biomass in cultures with urban wastewater, contributing to the treatment of sewage water.

$$\text{Oil (g)} = 0.4013 (\text{MO}) + 0.2141 \quad (8)$$

$$\text{Coagulant (g)} = 0.2583 (\text{MO}) + 0.2099 \quad (9)$$

Although no significant differences were observed ($P = 0.345$) in the content of the coagulant extracted under the two concentrations (5% and 10%) of extracting solution $(\text{NH}_4)_2\text{SO}_4$, all the extractions were used in the jar tests with the purpose of identifying the optimal dose and pH (Table 2), as well as the possible contaminant effect of the coagulant on the quality of the oil extracted from the algal biomass. The average content of coagulant extracted for the six samples showed a positive correlation ($R = 0.94$) with respect to the MO content (g); suggesting that approximately 0.47 g of coagulant could be obtained per gram of MO (w/w ; Equation (9)). The linearity shows an interception with the waste generated, suggesting that the extraction capacity of the extracting solution $(\text{NH}_4)_2\text{SO}_4$ tends to decrease as the raw material of MO increases, meaning that a part of the MO could still coagulated without reacting with the solution $(\text{NH}_4)_2\text{SO}_4$, producing higher excess residue. Therefore, under the operating conditions presented in this study, 4 g of MO and a volume of 50 mL of 5% or 10% $(\text{NH}_4)_2\text{SO}_4$ could satisfactorily extract coagulant (Figure 2).

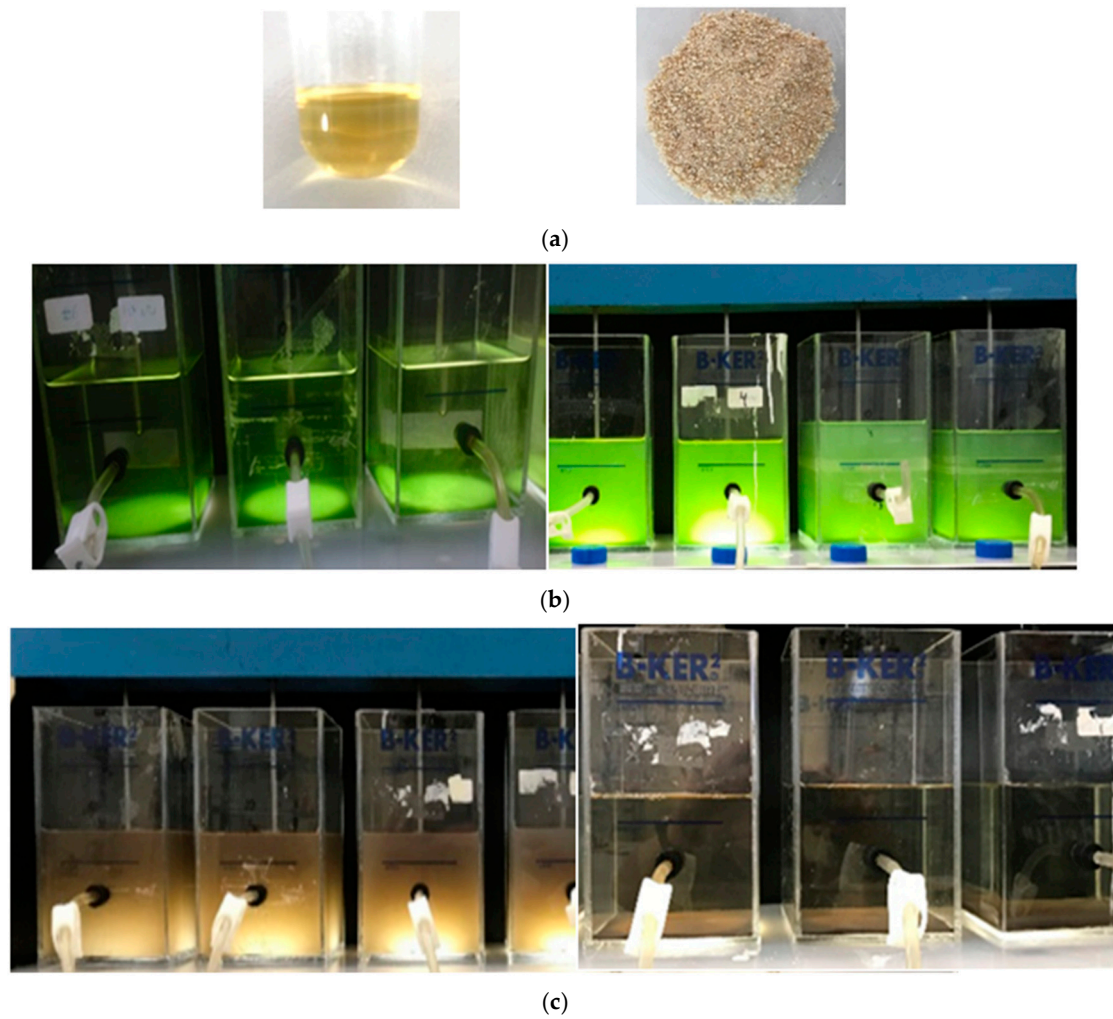


Figure 1. Jar test, dose determination, and optimal pH during the algal flocculation with urban wastewater: (a) Oil extraction from *Moringa oleifera* seed; (b) flocculation with microalgae culture; and (c) flocculation with urban wastewater.

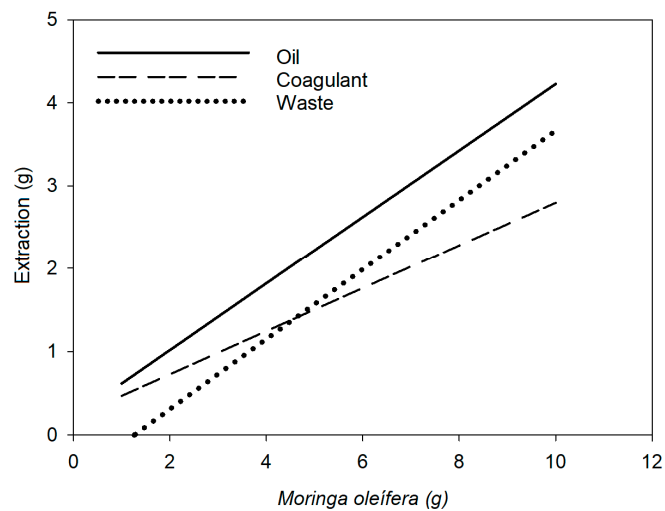


Figure 2. Linearity of the oil content (g) and biomass of *Moringa oleifera*.

Table 2. Flocculant content extracted from *Moringa oleifera* (g) per volume of extracted solution (mL).

<i>Moringa oleifera</i> (g)	$\frac{\text{g flocculant}}{\text{mL (NH}_4)_2\text{SO}_4}$		
	Solution (NH ₄) ₂ SO ₄		
	5%	10%	Average
1	0.009 ± 0.001 ^a	0.007 ± 0.001 ^a	0.008
2	0.016 ± 0.002 ^a	0.015 ± 0.001 ^a	0.015
4	0.029 ± 0.003 ^a	0.019 ± 0.007 ^a	0.024
6	0.036 ± 0.008 ^a	0.035 ± 0.005 ^a	0.035
8	0.051 ± 0.001 ^a	0.049 ± 0.001 ^a	0.050
10	0.059 ± 0.009 ^a	0.046 ± 0.002 ^a	0.052

Different letters indicate significant differences (Tukey, $P \leq 0.05$).

The coagulant dose is an important coagulation factor since it influences biomass recovery costs. The efficient coagulation–flocculation of the MO was determined based on the removal of microalgal biomass from urban wastewater to produce a clear supernatant. Cultures of *S. obliquus* in urban wastewater were treated at different flocculant doses: 0.38, 0.69, 1.23, 1.53, 1.92, and 2.61 g L⁻¹ (Table 2). The highest flocculation efficiency in algal culture was achieved at an optimum dose of 0.38 g L⁻¹, reaching 80.33% and 72.13% removal for the treatments with 5% and 10% extractive solution (NH₄)₂SO₄, respectively (Table 3). The low removal observed for a 10% saturated solution of (NH₄)₂SO₄ could be attributed to the excess of unreacted (NH₄)₂SO₄, changing the chemical characteristics of the water, producing a whitish coloration. It is therefore thought that the physical-chemical processes of coagulation–flocculation at the end of the treatment do not contribute surplus reagents that increase the nutrient content, and avoid the possible formation of chloramines in the treated effluents after disinfection.

Table 3. Flocculant dose (g L⁻¹) and final turbidity (% removal) obtained from the jar test in *S. obliquus* culture in urban wastewater.

$\frac{\text{g flocculant}}{\text{mL (NH}_4)_2\text{SO}_4}$	Dose (g L ⁻¹)	Turbidity (NTU)	Turbidity (NTU)	pH _{Final}
		Solution Extractor 5% (NH ₄) ₂ SO ₄	Solution Extractor 10% (NH ₄) ₂ SO ₄	
0.008	0.38	12 (80.33)	17 (72.13)	7.05
0.015	0.69	20 (67.21)	22 (63.93)	7.04
0.024	1.23	25 (59.02)	23 (62.30)	7.23
0.035	1.53	29 (52.46)	23 (62.30)	7.12
0.050	1.92	49 (19.67)	24 (60.66)	7.90
0.052	2.61	24 (60.66)	33 (45.90)	7.21

Note: NTU: nephelometric turbidity units; Initial turbidity (C₀): 61 NTU.

During the treatment of the cultures, increases in dose did not favor the sedimentation of algal biomass (Table 3). Similar results were reported by Abdul-Hamid et al. [6], who found that the efficient recovery of algal biomass *Chlorella* sp. is possible at a dose of 10 mg L⁻¹, concluding that dose increases result in poor recovery. Ndabigengesere and Narasiah [24] suggested that the addition of coagulant above the optimal dose leads to the formation of residual excess coagulant, since all the microalgae particles already form larger colloids.

For urban wastewater, the efficient removal of solids does not differ from the optimal dose obtained in *S. obliquus* cultures; likewise, increases in coagulant dose does not produce a significant increase in removal efficiency, suggesting that factors such as the concentration of solids and pH are factors that could affect the aggregation of particles (Table 4).

Table 4. Flocculant dose (g L^{-1}) and final turbidity (% removal) obtained from the jar test in urban wastewater.

$\frac{\text{g flocculant}}{\text{mL (NH}_4\text{)}_2\text{SO}_4}$	Dose (g L^{-1})	Turbidity (NTU)		pH _{Final}
		Sol. Extractor 5% (NH_4) ₂ SO ₄	Sol. Extractor 10% (NH_4) ₂ SO ₄	
0.008	0.38	9.6 (98.48)	36 (96.33)	6.5
0.015	0.69	11.5 (98.18)	28 (97.15)	6.6
0.024	1.23	16.0 (97.47)	21 (97.86)	6.7
0.035	1.53	19.0 (97.00)	20 (97.96)	6.6
0.050	1.92	25.5 (95.97)	19 (98.06)	6.6
0.052	2.61	29.6 (95.32)	20 (97.96)	6.6

Note: NTU: nephelometric turbidity units.

Beltran-Heredia et al. [25] reported an efficient removal of 50% in wastewater dyes for a low dose of 25 mg L^{-1} . Similarly, Sanchez-Martin et al. [20] reported a high rate of solids removal from the Meuse River in Rotterdam (The Netherlands) using a low dose of MO coagulant (0.5 mg L^{-1}), suggesting that a low dose is enough to improve the water quality.

Although the dose (0.38 g L^{-1}) reported here was higher than those reported in other studies, this dose is low compared to the other treatments, which proved to be efficient in algal cultures and urban wastewater, improving the water's temperature and reducing the one-step coagulant extraction process at a lower cost. Therefore, this dose can be obtained with only 1 g of MO (Tables 3 and 4), as can also be observed by comparing the coagulation efficiency using other coagulants (Table 5). This would support its potential application in algal crops for the biomass harvest and production of biodiesel or the extraction of high-value chemicals.

Table 5. Comparative efficiency and dose of flocculants in algal culture media and wastewater.

Coagulant–Flocculant	Treatment	Dose and Efficiency Removal (%)	Reference
<i>Moringa oleifera</i>	<i>Scenedesmus obliquus</i> cultivation	72.13–80.33%	Our study
	Urban wastewater	Dose: 0.38 g L^{-1} pH: 7–8 96–98%	
Chitosan	<i>Euglema gracilis</i> cultivation	Dose: 200 mg L^{-1} pH: 7–7.5	Gualteri et al. [26]
Chitosan	<i>Rhodomonas baltica</i> cultivation	75%	Lubian et al. [27]
Acetate	<i>Pleurochrysis carterae</i> cultivation	81–95%	Lee et al. [28]
Glucose		89–97%	
Glycerine		93–97%	
Magnafloc LT25, LT27	<i>Chaetoceros calcitrans</i> cultivation	82%	Harith et al. [29]
		Dose: $0.1\text{--}0.75 \text{ mg L}^{-1}$ pH: 8–10	
Chitosan	<i>Chaetoceros calcitrans</i> cultivation	83%	Harith et al. [29]
		Dose: 20 mg L^{-1} pH: 5–8	
Chitosan/aluminum sulfate	Urban Wastewater	74.3–98.2%	Bina et al. [30]
		Dose: $0.5\text{--}5 \text{ mg L}^{-1}$ pH: 7–7.5	

Another variable to study in the coagulation–flocculation process is pH. Experiments with different pH values were performed in *S. obliquus* cultures and urban wastewater, varying the pH between 8 and 13 with a fixed coagulant dose of 0.38 g L^{-1} . Tables 6 and 7 show the values of removal (%) versus pH. The highest efficiencies, 70.97% and 83.72%, were observed at pH 8–9 with 5% and 10% (NH_4)₂SO₄

solution, respectively. The changes at alkaline pH release the excess nitrogen in the form of N gas by shifting the pH chemical equilibrium to above 9. The tendency of a basic pH at the end of the treatment would explain the low removal efficiency and turbidity increase in the water by the formation of SO_4 . In practice, the pH variation in the wastewater is not significant; it is within the values of 8 and 9, so pH adjustments are not necessary for the removal of solids. According to Beltran-Heredia et al. [25], the effective pH for coagulation is in the range of 7 to 9, similar to the present study. This result was similar to that reported in other studies where coagulation–flocculation processes are pH-dependent, such as wastewater with high metal contents [31,32].

Table 6. Determining the optimal pH and final turbidity (% removal) obtained from the jar test in the microalgal culture at an optimum flocculant dose of 0.38 g L^{-1} .

pH	Turbidity (NTU)	Turbidity (NTU)	pH _{final}
	Sol. Extractor 5% (NH_4) ₂ SO ₄	Sol. Extractor 10% (NH_4) ₂ SO ₄	
8	5.7 (70.97)	8.8 (55.10)	7.25
9	3.2 (83.72)	7.5 (61.58)	7.66
10	2.6 (86.58)	5.8 (70.56)	8.23
11	2.7 (86.07)	5.7 (70.66)	8.48
12	2.3 (88.27)	3.6 (81.63)	9.37
13	3.6 (81.68)	1.1 (94.39)	12.76

Table 7. Determining the optimal pH and final turbidity (% removal) obtained from the jar test in urban wastewater at an optimum flocculant dose of 0.38 g L^{-1} .

pH	Turbidity (NTU)	Turbidity (NTU)	pH _{final}
	Sol. Extractor 5% (NH_4) ₂ SO ₄	Sol. Extractor 10% (NH_4) ₂ SO ₄	
8	4.9 (99.41)	16.0 (98.0)	8.1
9	3.1 (99.63)	15.0 (98.13)	9.2
10	4.2 (99.49)	18.0 (97.75)	9.5
11	4.3 (99.49)	9.0 (98.88)	10.3
12	3.6 (99.57)	7.0 (99.13)	12.3
13	3.4 (99.59)	2.0 (99.75)	13.1

At the end of the treatment period, the quality of the residual water in the *S. obliquus* cultures and only the residual waters (control), there were reductions in total solids (TDS) and biochemical oxygen demand (BOD) of approximately 95%. These concentrations are lower than those established by Mexican regulations (NOM-001-SEMARNAT, 1996); the maximum permissible limits for the control of wastewater discharge in estuaries and wetlands for SDT and BOD are 25 and 150 mg L^{-1} , respectively.

Methyl Esters Fatty Acids Profile (FAME)

The fatty acids profile for *Moringa oleifera*, in comparison to that obtained from biomass harvested from *S. obliquus* after flocculation, did not show significant differences ($P = 0.996$). This suggests that both oils have similar characteristics, with an SFA content of 36.24–36.54%, monounsaturated fatty acid (MUFA) content of 32.78–36.13%, and a polyunsaturated fatty acid (PUFA) content of 27.63–30.67% (Table 8). In particular, the activity of the flocculant on the quality properties of the oil obtained by *S. obliquus* could be observed as not having a significant effect for the synthesis of biodiesel (Table 9).

Table 8. Methyl Esters Fatty Acids Profile (FAME) (% w/w) of *Moringa oleifera* and microalgae *S. obliquus* harvested after flocculation.

FAME	<i>Moringa oleifera</i>	<i>Scenedesmus obliquus</i>
Butyric acid (C4: 0)	2.97	1.21
Caproic acid (C6: 0)	0.42	1.54
Caprylic acid (C8: 0))	0.61	1.26
Capric acid (C10: 0)	1.42	0.90
Undecanoic acid (C11: 0)	0.84	2.02
Lauric acid (C12: 0)	2.95	1.25
Tridecanoic acid (C13: 0)	2.14	0.92
Acid Miristic (C14: 0)	2.78	2.54
Pentadecanoic Acid (C15: 0)	2.37	3.93
Palmitic Acid (C16: 0)	3.16	2.25
Heptadecanoic Acid (C17: 0)	3.27	3.28
Stearic Acid (C18: 0)	3.33	2.16
Arachidic Acid (C20: 0)	1.32	1.39
Heneicosanoic acid (C21: 0)	3.42	3.86
Behenic acid (C22: 0)	2.53	3.88
Tricosanoic acid (C23: 0)	2.68	2.70
Lignoceric acid (C24: 0)	0	1.38
Miristoleic acid (C14: 1)	3.09	1.16
Cis-pentadecanoic acid (C15: 1)	3.15	1.19
Palmitoleic acid (C16: 1))	1.71	0.76
Cis-Heptadecanoic acid (C17: 1)	2.26	6.93
Elaidic acid (C18: 1N9T)	4.05	8.61
Oleic acid (C18: 1N9C)	4.79	3.18
Gadoleic acid (C20: 1)	2.34	1.15
Erucic acid (C22: 1N9)	6.05	1.38
Nervonic acid (C24: 1)	8.67	8.38
Linoleic acid (C18: 2N6T)	2.57	1.54
Linoelaidic acid (C18: 2N6C)	1.52	2.71
Linolenic acid (C18: 3N6)	6.21	3.49
α -Linolenic acid (C18: 3N3)	0.18	0.58
Eicosadienoic acid (C20: 2)	1.34	2.96
Dihomo- γ -Linolenic acid (C20: 3N6)	1.23	1.92
Eicosatrienoic acid (C20: 3N3)	0	0.92
Arachidonic Acid (C20: 4N6)	3.34	1.05
Docosaadienic Acid (C22: 2)	1.78	3.96
Eicosapentaenoic Acid (C20: 5N3)	3.16	5.54
Docosahexaenoic Acid (C22: 6N3)	6.28	5.97
SAF (% wt)	36.24	36.54
MUFA (% wt)	36.13	32.78
PUFA (% wt)	27.63	30.67
LCSF (% wt)	5.91	10.05
SFA/PUFA	1.3	1.2

SFA: saturated fatty acid, MUFA: monounsaturated fatty acid, PUFA: polyunsaturated fatty acid, LCSF: long chain saturation factor. Values are average of triplicates.

The SFA, MUFA, and PUFA contents affect the quality of biodiesel. An oil containing high concentrations of PUFA and MUFA compared with SFAs tends to produce biodiesel with a high iodine value and poor oxidative stability. However, this was not observed for the *S. obliquus* cultivated in domestic wastewater and *Moringa oleifera* seed (Table 8). Therefore, the quality parameters evaluated using the CN and SV were related to the saturation of FAME in both *M. oleifera* and *S. obliquus*.

The CN was low compared with the value recommended by international standards ASTM 6751 and EN14214 (Table 9) for both microalgae and *M. oleifera*. Our studies suggest that high cetane number and proportions of SFA could be associated with efficient combustion properties of biodiesel, similar to those reported by other authors [33,34]. Wu and Miao [28] reported a CN for *S. obliquus* positively

correlated with the SFA content and negatively correlated with DU, suggesting good ignition of the fuel when the SFA/PUFA ratio is approximately 2.31–4.02. For *S. obliquus* and *M. oleifera*, the SFA/PUFA ratios were low at 1.2–1.3 (Table 8), indicating good ignition of biodiesel. The SFA amount with respect to the PUFA amount may provide the best indication of the good ignition of a biodiesel; conversely, a high percentage of SFA affects the flow properties, causing the crystallization and solidification of the fuel in engine filters under colder climatic conditions [35]. An analysis of the biodiesel produced by *S. obliquus* where the SFAs and MUFAs dominate suggest poor cold flow properties; therefore, the use of this biodiesel in cold climate conditions may be limited. This problem could be minimized by mixing with oil from other species with opposite characteristics [23]. For *M. oleifera*, we propose its use as a biodiesel in practical applications in warm climates.

The iodine value (IV) is related to the oxidative stability, implying that biodiesel with high IV values are less stable to oxidation [36]. In the present study, the biodiesel obtained by *S. obliquus* and *M. oleifera* showed IV values close to 120 g I₂ 100 g⁻¹ lipids, and an oxidative stability (OS) value within three to six minutes according to the values established by the European standard (Table 8). The IV, DU, CFPP, and OS values in comparison with other studies for *S. obliquus* are similar, within the range established by ASTM D6751 and EN 14,214 standards (Table 9) [21–23,33,37,38], suggesting that the biodiesel obtained from the harvested *S. obliquus* using *M. oleifera* bioflocculants has good oxidative stability. This also suggests that the bioflocculant did not negatively affect the biodiesel quality. In accordance with other studies (Table 9) [21–23,33,37,38], we conclude that oil rich in SFA will generate biodiesel with high CN, low IV, and high oxidative stability, whereas oils with high PUFA content (high DU) will produce biodiesel with low CN and high IV, and will be more prone to oxidation.

Table 9. The physico-chemical properties of *Scenedesmus obliquus* base biodiesel production compared with international standards and those in other studies.

Biodiesel Properties	Units	ASTM D6751	EN 14214	[37]	[33]	[21]	[23]	[22]	[38]	<i>S. obliquus</i>	<i>M. oleifera</i>
CN	min	47	51	59.98	57.93	57.13	63.63	51.74	40.2	45.75	45.43
IV	g I ₂ 100 g ⁻¹	-	120	77.36	72.81	77.91	35.38	98.86	27.2	119.64	117.52
CFPP	°C	-	≤5 ≤ -20	-3.19	-5.68	-0.04	-11.87	3.5	-7.1	2.08	15.09
SV	mg KOH g ⁻¹	-	-	164.6	194.8	192.4	216.0	-	315.3	206.95	213.44
DU	% wt	-	-	87.04	83.97	-	36.63	-	30.83	94.13	91.38
OS	h	3	6	7.31	-	-	-	3.53	6.6	4.15	4.26

CN: cetane number; IV: iodine value; CFPP: cold filter plugging point; SV: saponification value; DU: degree of unsaturation; OS: oxidative stability; SFA: saturated fatty acid; MUFA: monounsaturated fatty acid; PUFA: polyunsaturated fatty acid. Values are average of triplicates.

4. Conclusions

The growing demand for chemical coagulants for wastewater treatment has led to the search for new sources of cost-effective organizer coagulants to reduce the impacts of wastewater on ecosystems. The *Moringa oleifera* seed shows potential as a low cost coagulant–flocculant that could be used in harvesting the microalgae that grows in urban wastewater, in addition to improving the quality of the effluents emitted from treatment plants. In the present study, the extraction of flocculant with 5% (NH₄)₂SO₄ solution without purification achieved 80.33% removal with a low dose of 0.38 g L⁻¹. Enough flocculant (0.47 g flocculant) was obtained from 1 g of *M. oleifera*. The extracting solution of (NH₄)₂SO₄ at 10% produces excess nitrogen that is released in the form of N gas at basic pH values (above 9), producing whitish turbidity.

The oil profile (MO and *S. obliquus*) showed contents of saturated fatty acids (SFA) of 36.24–36.54%, monounsaturated fatty acids of 32.78–36.13%, and polyunsaturated fatty acids of 27.63–30.67%. The biodiesel produced by *S. obliquus* and harvested from urban wastewater showed that when the SFAs dominate the MUFAs, the biodiesel has poor cold flow properties. Therefore, this application of

this biodiesel in cold climates may be limited, although this problem can be minimized by mixing it with oil from other species with opposite characteristics. *M. oleifera* is proposed for use as a biodiesel in warm climates. For both oils, the high cetane number (CN) is positively correlated with high SFA content and negatively correlated with the degree of saturation (DU), suggesting good fuel ignition and good oxidative stability properties, likewise suggesting that the bioflocculant negatively affects the biodiesel's quality. This makes MO a potentially harmless bioflocculant for microalgal harvesting in urban wastewater, contributing to the treatment of wastewater and providing a possible source of low-cost biodiesel.

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